



## Description

### Technical Field

[0001] The present invention relates to a refrigerating apparatus having supercritical refrigerating cycles using as a refrigerant a natural system refrigerant, which apparatus is suitable to be used for, for example, a heat-source unit of heat pump type hot-water supply equipment.

### Background Art

[0002] Heat pump type hot-water supply equipment is equipped with, in general, a tank unit 71 having a hot-water reservoir tank 70, and a heat-source unit 73 having a refrigerant circuit 72, as shown in Fig. 7. The refrigerant circuit 72 is so configured as to connect a compressor 74, a hydrothermal exchanger 75, an expansion valve 77, and an evaporator 78 in order. The tank unit 71 includes the hot-water reservoir tank 70 and a circulation path 79. The circulation path 79 is provided with a pump 80 for water circulation and a heat exchange path 81 which constitutes a part of the hydrothermal exchanger 75.

[0003] Here, the operation of the aforementioned heat pump type hot-water supply equipment will be described.

[0004] First, the compressor 74 is driven while the pump 80 for water circulation is also driven (operated). Then, stored water (hot water) flows out from the water intake provided at the bottom of the hot-water reservoir tank 70 to the circulation path 79, and the hot-water flown out flows through the heat exchange path 81. Here, the hot water flowing through the heat exchange path 81 is heated (boiled) by the hydrothermal exchanger 75. The hot water heated flows into the top portion of the hot-water reservoir tank 70 from the hot-water inlet. Thereby, the hot water of high temperature is stored in the hot-water reservoir tank 70.

[0005] Conventionally, as a refrigerant circulating the refrigerant circuit, such a refrigerant as dichlorodifluoromethane (R-12) or chlorodifluoromethane (R-22) was used. However, from the point of preventing destruction of the ozone layer, preventing environmental pollution, and the like, an alternative refrigerant such as 1,1,1,2-tetrafluoro ethane (R-134a) has been used as a refrigerant. Still, the alternative refrigerant such as R-134a has a problem of having a high ability to cause a greenhouse effect or the like. Therefore, it has been gradually recommended in recent years to use a natural system refrigerant, which is free of the aforementioned defect, as a refrigerant. As a natural system refrigerant of this kind, carbon dioxide, for example, is well known.

[0006] As the outside air temperature varies along with the season's transition, a load change occurs in the aforementioned equipment. According to the load change, the refrigerant cycles also change. This means

that the preferable amount of circulated refrigerant is different for every season. Thus, it has been difficult to operate with the optimum amount of circulated refrigerant unless some measures are taken. If the actual amount of the circulated refrigerant is less than the optimum amount of the circulated refrigerant, the superheated refrigerant is sucked into the compressor 74, causing the compressor 74 to be operated in the excessively superheated condition. In contrast, if the actual amount of the circulated refrigerant exceeds the optimum amount of the circulated refrigerant, the refrigerant, which has not been evaporated completely, is sucked into the compressor 74, causing the compressor 74 to be operated in the wet condition. As a result, the reliability of the compressor 74 is degraded.

[0007] The present invention is developed to solve the aforementioned conventional problems. The object of the present invention is to provide a technique which enables to operate with a proper amount of circulated refrigerant by controlling the amount, and prevents an excessive superheat operation or a wet operation.

### Disclosure of the Invention

[0008] A first refrigerating apparatus devised by the present invention comprises: a supercritical freezing cycle R having a compressor 25 for compressing a refrigerant to a pressure higher than the critical pressure, a gas cooler 26, a decompressing mechanism 27 and an evaporator 28, and using as the refrigerant a natural system refrigerant; a receiver 43 provided to the high-pressure side of the supercritical freezing cycle R; a receiver temperature detector 50a for detecting the temperature of the receiver 43; and a controller 55 for controlling the amount of the circulated refrigerant by bringing the temperature of the receiver 43 detected by the receiver temperature detector 50a close to a target receiver temperature.

[0009] In the aforementioned first refrigerating apparatus, the controller 55 controls the temperature of the receiver 43 so as to come close to the target receiver temperature set corresponding to, for example, the season, whereby the refrigerant temperature in the receiver 43 can be adjusted. This enables to control the density of the refrigerant in the receiver 43. As a result, the refrigerant amount stored in the receiver 43 can be adjusted. Therefore, the refrigerant amount stored in the receiver 43 can be made to the amount corresponding to the season, whereby the amount of the circulated refrigerant can be made to the amount corresponding to the season. Therefore, an excessive superheat operation and a wet operation can be prevented.

[0010] A second refrigerating apparatus devised by the present invention comprises an outside air temperature detector 53a for detecting the outside air temperature, and the controller 55 thereof is so configured as to calculate the target receiver temperature based on the outside air temperature detected by the outside air

temperature detector **53a**.

**[0011]** In the aforementioned second refrigerating apparatus, the controller **55** calculates the target receiver temperature based on the outside air temperature serving as an index for controlling the amount of the circulated refrigerant. Therefore, it is ensured that the amount of the circulated refrigerant is made to the expected amount (for example, the amount of the circulated refrigerant corresponding to the season).

**[0012]** Further, since the outside air temperature is detected by the outside air temperature detector **53a**, the outside air temperature can be detected without a computation. Therefore, if the target receiver temperature is calculated based on the outside air temperature, it is possible to simplify the computation for controlling the amount of the circulated refrigerant.

**[0013]** A third refrigerating apparatus devised by the present invention comprises a superheat degree detector **51a**, **52a**, **55** for detecting the superheat degree of the refrigerant at the outlet of the evaporator **28**, and the controller **55** thereof is so configured as to calculate the target receiver temperature based on the superheat degree detected by the superheat degree detector **51a**, **52a**, **55**.

**[0014]** In the third refrigerating apparatus, the controller **55** calculates the target receiver temperature based on the superheat degree serving as an index for controlling the amount of the circulated refrigerant. Therefore, it is ensured that the amount of the circulated refrigerant is made to the expected amount (for example, the amount of the circulated refrigerant corresponding to the season).

**[0015]** Further, the magnitude of the superheat degree has a close relationship with the degree of the superheat operation. Therefore, if the target receiver temperature is calculated based on the superheat degree, it is possible to control the amount of the circulated refrigerant with high precision.

**[0016]** A forth refrigerating apparatus devised by the present invention comprises, an outside air temperature detector **53a** for detecting the outside air temperature, and a superheat degree detector **51a**, **52a**, **55** for detecting the superheat degree of the refrigerant at the outlet of the evaporator **28**, and the controller **55** thereof is so configured as to calculate the target receiver temperature based on the outside air temperature detected by the outside air temperature detector **53a** and the superheat degree detected by the superheat degree detector **51a**, **52a**, **55**.

**[0017]** In the aforementioned forth refrigerating apparatus, the controller **55** calculates the target receiver temperature based on the outside air temperature and the superheat degree serving as indexes for controlling the amount of the circulated refrigerant. Therefore, it is ensured that the amount of the circulated refrigerant is made to the expected amount (for example, the amount of the circulated refrigerant corresponding to the season).

**[0018]** Further, if the target receiver temperature is calculated based on the outside air temperature and the superheat degree, the target receiver temperature is calculated based on the two indexes, whereby it is possible to control the amount of the circulated refrigerant with high precision.

**[0019]** A fifth refrigerating apparatus devised by the present invention comprises an adjusting valve **44** for adjusting the amount of the refrigerant flowing through the inside of the receiver **43**, and the controller **55** thereof is so configured as to adjust the opening of the adjusting valve **44** to thereby bring the temperature of the receiver **43** detected by the receiver temperature detector **50a** close to the target receiver temperature.

**[0020]** In the aforementioned fifth refrigerating apparatus, the controller **55** brings the temperature of the receiver **43** close to the target receiver temperature by adjusting the opening of the adjusting valve **44**. Therefore, with a simple control of adjusting the opening of the adjusting valve **44**, the amount of the circulated refrigerant can be controlled.

**[0021]** A sixth refrigerating apparatus devised by the present invention comprises: a supercritical freezing cycle **R** having a compressor **25** for compressing a refrigerant to a pressure higher than the critical pressure, a gas cooler **26**, a decompressing mechanism **27** and an evaporator **28**, and using as the refrigerant a natural system refrigerant; a receiver **43** provided to the high-pressure side of the supercritical freezing cycle **R**; an adjusting valve **44** for adjusting the amount of the refrigerant flowing through the inside of the receiver **43**; an outside air temperature detector **53a** for detecting the outside air temperature; and a controller **55** for controlling the amount of the circulated refrigerant by adjusting the opening of the adjusting valve **44** based on the outside air temperature detected by the outside air temperature detector **53a**.

**[0022]** In the aforementioned sixth refrigerating apparatus, the controller **55** adjusts the opening of the adjusting valve **44** based on the outside air temperature serving as an index for controlling the amount of the circulated refrigerant. Thereby, the refrigerant amount stored in the receiver **43** (refrigerant amount flowing through the inside of the receiver **43**) can be adjusted. Therefore, the amount of the circulated refrigerant can be made to the expected amount, whereby an excessive superheat operation and a wet operation can be prevented.

**[0023]** Further, since the outside air temperature is detected by the outside air temperature detector **53a**, the outside air temperature can be detected without a computation. Therefore, if the opening of the adjusting valve **44** is adjusted based on the outside air temperature, it is possible to simplify the computation for controlling the amount of the circulated refrigerant.

**[0024]** A seventh refrigerating apparatus devised by the present invention comprises: a supercritical freezing cycle **R** having a compressor **25** for compressing a re-

frigerant to a pressure higher than the critical pressure, a gas cooler 26, a decompressing mechanism 27 and an evaporator 28, and using as the refrigerant a natural system refrigerant; a receiver 43 provided to the high-pressure side of the supercritical freezing cycle R; an adjusting valve 44 for adjusting the amount of the refrigerant flowing through the inside of the receiver 43; a superheat degree detector 51a, 52a, 55 for detecting the superheat degree of the refrigerant at the outlet of the evaporator 28; and a controller 55 for controlling the amount of the circulated refrigerant by adjusting the opening of the adjusting valve 44 based on the superheat degree detected by the superheat degree detector 51a, 52a, 55.

[0025] In the aforementioned seventh refrigerating apparatus, the controller 55 adjusts the opening of the adjusting valve 44 based on the superheat degree serving as an index for controlling the amount of the circulated refrigerant. Thereby, the refrigerant amount stored in the receiver 43 (refrigerant amount flowing through the inside of the receiver 43) can be adjusted. Therefore, the amount of the circulated refrigerant can be made to the expected amount, whereby an excessive superheat operation and a wet operation can be prevented.

[0026] Further, the magnitude of the superheat degree has a close relationship with the degree of the superheat operation. Therefore, if the opening of the adjusting valve 44 is adjusted based on the superheat degree, the amount of the circulated refrigerant can be controlled with high precision.

[0027] An eighth refrigerating apparatus devised by the present invention comprises: a supercritical freezing cycle R having a compressor 25 for compressing a refrigerant to a pressure higher than the critical pressure, a gas cooler 26, a decompressing mechanism 27, and an evaporator 28, and using as the refrigerant a natural system refrigerant; a receiver 43 provided to the high-pressure side of the supercritical freezing cycle R; an adjusting valve 44 for adjusting the amount of the refrigerant flowing through the inside of the receiver 43; an outside air temperature detector 53a for detecting the outside air temperature; a superheat degree detector 51a, 52a, 55 for detecting the superheat degree of the refrigerant at the outlet of the evaporator 28; and a controller 55 for controlling the amount of the circulated refrigerant by adjusting the opening of the adjusting valve 44 based on the outside air temperature detected by the outside air temperature detector 53a and the superheat degree detected by the superheat degree detector 51a, 52a, 55.

[0028] In the aforementioned eighth refrigerating apparatus, the controller 55 adjusts the opening of the adjusting valve 44 based on the outside air temperature and the superheat degree serving as indexes for controlling the amount of the circulated refrigerant. Thereby, the refrigerant amount stored in the receiver 43 (refrigerant amount flowing through the inside of the receiver 43) can be adjusted. Therefore, the amount of the cir-

culated refrigerant can be made to the expected amount, whereby an excessive superheat operation and a wet operation can be prevented.

[0029] Further, if the opening of the adjusting valve 44 is adjusted based on the outside air temperature and the superheat degree, the target receiver temperature is calculated based on the two indexes, whereby the amount of the circulated refrigerant can be controlled with high precision.

[0030] A ninth refrigerating apparatus devised by the present invention comprises: an adjusting valve 44 for adjusting the amount of the refrigerant flowing through the inside of the receiver 43, and an outside air temperature detector 53a detecting the outside air temperature, and the controller 55 thereof is so configured as to correct from time to time during operation the target receiver temperature based on the outside air temperature, and adjust from time to time during operation the opening of the adjusting valve 44, to thereby bring the temperature of the receiver 43 close to the target receiver temperature corrected.

[0031] In the aforementioned ninth refrigerating apparatus, the controller 55 corrects from time to time during operation the target receiver temperature based on the outside air temperature, and adjusts from time to time during operation the opening of the adjusting valve 44 corresponding to the target receiver temperature corrected. Thereby, it is ensured to bring the temperature of the receiver 43 close to the target receiver temperature corrected. Therefore, the refrigerant amount stored in the receiver 43 can be made to the amount corresponding to, for example, the season, and the amount of the circulated refrigerant can be made to the amount corresponding to the season, whereby an excessive superheat operation and a wet operation can be prevented.

[0032] A tenth refrigerating apparatus devised by the present invention comprises: an adjusting valve 44 for adjusting the amount of the refrigerant flowing through the inside of the receiver 43, and a superheat degree detector 51a, 52a, 55 for detecting the superheat degree of the refrigerant at the outlet of the evaporator 28, and the controller 55 thereof is so configured as to correct from time to time during operation the target receiver temperature based on the superheat degree, and adjust from time to time during operation the opening of the adjusting valve 44, to thereby bring the temperature of the receiver 43 close to the target receiver temperature corrected.

[0033] In the aforementioned tenth refrigerating apparatus, the controller 55 corrects from time to time during operation the target receiver temperature based on the superheat degree, and adjusts from time to time during operation the opening of the adjusting valve 44 corresponding to the target receiver temperature corrected. Thereby, it is ensured to bring the temperature of the receiver 43 close to the target receiver temperature corrected. Therefore, the refrigerant amount stored in the

receiver 43 can be made to the amount corresponding to, for example, the season, and the amount of the circulated refrigerant can be made to the amount corresponding to the season, whereby an excessive superheat operation and a wet operation can be prevented.

[0034] An eleventh refrigerating apparatus according to the present invention comprises: an adjusting valve 44 for adjusting the amount of the refrigerant flowing through the inside of the receiver 43; an outside air temperature detector 53a for detecting the outside air temperature; and a superheat degree detector 51a, 52a, 55 for detecting the superheat degree of the refrigerant at the outlet of the evaporator 28; and the controller 55 thereof is so configured as to correct from time to time during operation the target receiver temperature based on the outside air temperature and the superheat degree, and adjust from time to time during operation the opening of the adjusting valve 44 to thereby bring the temperature of the receiver 43 close to the target receiver temperature corrected.

[0035] In the aforementioned eleventh refrigerating apparatus, the controller 55 corrects from time to time during operation the target receiver temperature based on the outside air temperature and the superheat degree, and adjusts from time to time during operation the opening of the adjusting valve 44 corresponding to the target receiver temperature corrected. Thereby, it is ensured to bring the temperature of the receiver 43 close to the target receiver temperature corrected. Therefore, the refrigerant amount stored in the receiver 43 can be made to the amount corresponding to, for example, the season, and the amount of the circulated refrigerant can be made to the amount corresponding to the season, whereby an excessive superheat operation and a wet operation can be prevented.

[0036] Each of a twelfth through a fifteenth refrigerating apparatuses devised by the present invention comprises, a bypass circuit 42 for connecting an intermediate portion of the high-pressure side of the supercritical freezing cycle R and a downstream portion located at the downstream side of the intermediate portion. The receiver 43 is provided to the bypass circuit 42, and the adjusting valve 44 is provided in between the receiver 43 and the downstream portion in the bypass circuit 42.

[0037] In each of the aforementioned twelfth through fifteenth refrigerating apparatuses, since the adjusting valve 44 is provided in between the receiver 43 and the downstream portion in the bypass circuit 42, the controller 55 can surely control the refrigerant amount stored in the receiver 43 provided to the bypass circuit 42, by adjusting the opening of the adjusting valve 44, whereby the amount of the circulated refrigerant can be surely made to the expected amount.

[0038] Each of a sixteenth through a nineteenth refrigerating apparatuses devised by the present invention comprises, a heat exchanger S for causing a heat exchange between the receiver 43 and the low-pressure refrigerant flowing through a passage 47 in the low-pres-

sure side of the supercritical freezing cycle R.

[0039] In each of the aforementioned sixteenth through nineteenth refrigerating apparatuses, the receiver 43 (the high-pressure refrigerant in the receiver 43) and the low-pressure refrigerant flowing through the passage in the low-pressure side of the supercritical freezing cycle R perform a heat exchange by the heat exchanger S, whereby the receiver 43 (the high-pressure refrigerant) can be cooled by the low-pressure refrigerant. Therefore, it is possible to easily bring the temperature of the receiver 43 (the high-pressure refrigerant) close to the target receiver temperature using the low-pressure refrigerant, without any additional cooler.

## 15 Effects

[0040] According to the aforementioned first refrigerating apparatus, the controller brings the receiver temperature close to the target receiver temperature, whereby the refrigerant amount stored in the receiver can be made to the amount corresponding to, for example, the season, whereby the amount of the circulated refrigerant can be made to the proper amount. Consequently, it is possible to operate the apparatus with the optimum amount of the circulated refrigerant through the year, whereby an excessive superheat operation and a wet operation can be prevented. This secures the reliability of the compressor. Further, by controlling the amount of the circulated refrigerant, a system such as heat pump type hot-water supply equipment having this refrigerating apparatus can exhibit maximum ability.

[0041] According to the aforementioned second refrigerating apparatus, the controller brings the receiver temperature close to the target receiver temperature, whereby it is ensured that the amount of the circulated refrigerant is made to the expected amount (the amount of the circulated refrigerant corresponding to the season), and also a stable operation can be made. Further, if the target receiver temperature is calculated based on the outside air temperature, the amount of the circulated refrigerant can be easily controlled.

[0042] According to the aforementioned third refrigerating apparatus, the controller brings the receiver temperature close to the target receiver temperature, whereby it is ensured that the amount of the circulated refrigerant is made to the expected amount (the amount of the circulated refrigerant corresponding to the season), and also a stable operation can be made. Further, if the target receiver temperature is calculated based on the superheat degree, the amount of the circulated refrigerant can be controlled with high precision.

[0043] According to the aforementioned fourth refrigerating apparatus, the controller brings the receiver temperature close to the target receiver temperature, whereby it is ensured that the amount of the circulated refrigerant is made to the expected amount (the amount of the circulated refrigerant corresponding to the season), and also a stable operation can be made. Further,

if the target receiver temperature is calculated based on the outside air temperature and the superheat degree, the amount of the circulated refrigerant can be controlled with higher precision.

[0044] According to the aforementioned fifth refrigerating apparatus, the controller brings the receiver temperature close to the target receiver temperature by adjusting the opening of the adjusting valve, whereby the amount of the circulated refrigerant can be easily controlled. Further, since the control for bringing the receiver temperature close to the target receiver temperature is such a simple control as adjusting the opening of the adjusting valve, the controller can be simplified. This leads to a reduction in the cost of the refrigerating apparatus.

[0045] According to the aforementioned sixth refrigerating apparatus, it is ensured that the amount of the circulated refrigerant can be made to the expected amount, whereby an excessive superheat operation and a wet operation can be prevented. This secures the reliability of the compressor. Further, by controlling the amount of the circulated refrigerant, a system such as heat pump type hot-water supply equipment having this refrigerating apparatus can exhibit maximum ability. Moreover, if the opening of the adjusting valve is adjusted based on the outside air temperature, it is possible to simplify the computation for controlling the amount of the circulated refrigerant.

[0046] According to the aforementioned seventh refrigerating apparatus, it is ensured that the amount of the circulated refrigerant can be made to the expected amount, whereby an excessive superheat operation and a wet operation can be prevented. This secures the reliability of the compressor. Further, by controlling the amount of the circulated refrigerant, a system such as heat pump type hot-water supply equipment having this refrigerating apparatus can exhibit maximum ability. Moreover, if the opening of the adjusting valve is adjusted based on the superheat degree, it is possible to control the amount of the circulated refrigerant with high precision.

[0047] According to the aforementioned eighth refrigerating apparatus, it is ensured that the amount of the circulated refrigerant can be made to the expected amount, whereby an excessive superheat operation and a wet operation can be prevented. This secures the reliability of the compressor. Further, by controlling the amount of the circulated refrigerant, a system such as heat pump type hot-water supply equipment having this refrigerating apparatus can exhibit maximum ability. Moreover, if the opening of the adjusting valve is adjusted based on the outside air temperature and the superheat degree, it is possible to control the amount of the circulated refrigerant with higher precision.

[0048] According to the ninth through eleventh refrigerating apparatuses described above, it is possible to surely bring the receiver temperature close to the target receiver temperature. Therefore, the refrigerant amount

stored in the receiver can be made to the amount corresponding to the season, and the amount of the circulated refrigerant can be made to the proper amount. This can surely prevent an excessive superheat operation and a wet operation, and secure the reliability of the compressor. Further, by controlling the amount of the circulated refrigerant, a system such as heat pump type hot-water supply equipment having this refrigerating apparatus can exhibit maximum ability.

[0049] According to the twelfth through fifteenth refrigerating apparatuses described above, the controller adjusts the opening of the adjusting valve, whereby the refrigerant amount flowing through the inside of the receiver provided to the bypass circuit (the refrigerant amount stored in the receiver) can be surely controlled. Therefore, it is ensured that the amount of the circulated refrigerant corresponding to the season can be obtained, so that an excessive superheat operation and a wet operation can be prevented.

[0050] According to the sixteenth through nineteenth refrigerating apparatus described above, it is possible to easily bring the receiver temperature close to the target receiver temperature using the low-pressure refrigerant flowing through a passage in the low-pressure side of the supercritical freezing cycle, without any additional cooler. Therefore, it is ensured that the amount of the circulated refrigerant corresponding to the season can be obtained, so that an excessive superheat operation and a wet operation can be prevented. Further, the configuration of the refrigerating apparatus can be simplified since no additional cooler is required.

#### Brief Description of the Drawings

##### [0051]

Fig. 1 is a schematic diagram showing heat pump type hot-water supply equipment according to an embodiment.

Fig. 2 is a schematic block diagram showing a control unit of a refrigerant circuit according to the embodiment.

Fig. 3 is a flowchart showing operating processes of the refrigerant circuit according to the embodiment.

Fig. 4 is a schematic diagram showing a receiver of the refrigerant circuit according to the embodiment.

Fig. 5 is a schematic diagram showing a deformation example of the receiver of the refrigerant circuit according to the embodiment.

Fig. 6 is a diagram showing the relationship among outside air temperatures, superheat degrees of the refrigerant of the outlet of the evaporator, target receiver temperatures, and the amount of refrigerant stored in the receiver.

Fig. 7 is a schematic diagram showing conventional heat pump type hot-water supply equipment.

### Best Mode for Carrying Out the Invention

[0052] Next, a specific embodiment of a refrigerating apparatus according to the present invention will be explained in detail with reference to the drawings. Fig. 1 shows a schematic diagram of heat pump type hot-water supply equipment using a refrigerating apparatus according to the present invention. This heat pump type hot-water supply equipment is equipped with a tank unit 1 and a heat source unit 2, and heats water (hot water) of the tank unit 1 by the heat source unit 2.

[0053] The tank unit 1 includes a hot-water reservoir tank 3, and the hot water stored in the hot-water reservoir tank 3 is supplied to, for example, a bath tub (not shown). Thus, in the hot-water reservoir tank 3, there are provided a water supply opening 5 to the bottom wall thereof, and a tapping hole 6 to the upper wall thereof. Water is supplied from the water supply opening 5 to the hot-water reservoir tank 3, and hot water of high temperature is supplied from the tapping hole 6. Further, in the hot-water reservoir tank 3, there are provided a water intake 10 to the bottom wall thereof, and a hot-water inlet 11 to the upper part of the side wall (peripheral wall). The water intake 10 and the hot-water inlet 11 are connected via a circulation path 12. The circulation path 12 is provided with a pump 13 for water circulation and a heat exchange path 14. Further, a channel 8 for water supply is connected to the water supply opening 5.

[0054] The heat source unit 2 is provided with a refrigerant circuit R according to the present embodiment. This refrigerant circuit R is so configured as to connect, a compressor 25 for compressing a refrigerant to a pressure higher than the critical pressure, a hydrothermal exchanger (gas cooler) 26 having the heat exchange path 14, a motor-operated expansion valve (decompressing mechanism) 27, and an air heat exchanger (evaporator) 28, in order. That is, the compressor 25 and the gas cooler 26 are connected via a discharge pipe (refrigerant passage) 29, the gas cooler 26 and the motor-operated expansion valve 27 are connected via a refrigerant passage 30, the motor-operated expansion valve 27 and the evaporator 28 are connected via a refrigerant passage 31, and the evaporator 28 and the compressor 25 are connected via a suction pipe (refrigerant passage) 33 having an accumulator 32. As a refrigerant, a natural system refrigerant such as carbon dioxide (CO<sub>2</sub>) is used. Note that the gas cooler 26 used as a hydrothermal exchanger has a function of cooling a refrigerant of high temperature and high pressure which has been compressed in the compressor 25. Further, to the discharge pipe 29, an HPS 40 used as a pressure protection switch and a pressure sensor 41 are provided.

[0055] Further, the refrigerant circuit R is provided with a liquid-gas heat exchanger 34 for cooling the refrigerant of high pressure and high temperature flown out from the gas cooler 26. The liquid-gas heat exchanger 34 has, for example, a double pipe structure which

includes a first passage 35 through which the refrigerant flown out from the gas cooler 26 flows, and a second passage 36 through which the refrigerant flown out from the evaporator 28 flows. That is, the first passage 35 forms a part of the refrigerant passage 30, and the second passage 36 forms a part of the suction pipe 33. With this structure, the refrigerant of high pressure and high temperature flowing through the first passage 35 and the refrigerant of low pressure and low temperature flowing through the second passage 36 perform a heat exchange. Then, the refrigerant flown out from the gas cooler 26 is supercooled. Further, the refrigerant before flown into the accumulator 32 is heated. As such, a wet operation can be prevented.

[0056] Further, the refrigerant circuit R is provided with a defrost bypass circuit 38 for connecting the discharge pipe 29 and the refrigerant passage 31. The defrost bypass circuit 38, having a defrost valve 39, is used to perform a defrost operation for supplying hot gas discharged from the compressor 25 to the evaporator 28 so as to remove frost on the evaporator 28. For this purpose, the heat source unit 2 is provided with a defrost control device (not shown) which switches between the normal water heating operation and the defrost operation. In a case that the water heating operation is performed as a normal operation, the gas cooler 26 works as a condenser so as to heat hot water flowing through the heat exchange path 14. On the other hand, in a case that the defrost operation is performed, the motor-operated expansion valve 27 is set to a predetermined opening and the defrost valve 39 is set to be in the opening state, whereby hot gas flows into the evaporator 28. Then, the evaporator 28 is heated by the hot gas, so that frost on the evaporator 28 is removed. Note that the defrost control device is formed of a microcomputer, for example.

[0057] Further, the refrigerant circuit R is branched at the high-pressure side, and is provided with a bypass circuit 42 for connecting the branch portion and the downstream portion located downstream of the branch portion. The bypass circuit 42 has a receiver 43. In between the receiver 43 and the downstream portion in the bypass circuit 42, there is provided an adjusting valve 44 for adjusting flow rate. In other words, the bypass circuit 42 includes, a first passage 45 connecting the upstream portion of the gas cooler 26 and the receiver 43, and a second passage 46 connecting the downstream portion located downstream of the upstream portion of the gas cooler 26 and the receiver 43, and the second passage 46 is provided with the adjusting valve 44.

[0058] In the receiver 43, there is provided a passage 47 which forms a part of the refrigerant passage 31, as shown in Fig. 4. The receiver 43 (the high-pressure refrigerant flown into the receiver 43 via the bypass circuit 42) and the low-pressure refrigerant flowing through the passage 47 perform a heat exchange. That is, the low-pressure refrigerant flowing through the passage 47 constitutes a cooler (heat exchanger) S for bringing the



temperature of the receiver 43 (high-pressure refrigerant in the receiver 43) close to the target receiver temperature which will be described below.

[0059] The target receiver temperature is, for example, determined corresponding to the season. When the temperature of the receiver 43 comes close to the target receiver temperature, the equipment can be operated with the optimum amount of the circulated refrigerant, so that an excessive superheat operation and a wet operation can be prevented. The target receiver temperature is determined corresponding to the season by performing a preliminary test or the like beforehand using the heat pump type hot-water supply equipment.

[0060] As shown in Fig. 2, the control unit of the heat pump type hot-water supply equipment includes, a receiver temperature detector 50, an air heat exchanger temperature detector 51, a suction pipe temperature detector 52, an outside air temperature detector 53, setting means 54 for setting the target receiver temperature, and a controller 55 into which data (value) from each of the detectors 50, 51, 52, 53 and the setting means 54 is input.

[0061] The controller 55 adjusts the opening of the adjusting valve 44. By adjusting the opening of the adjusting valve 44 so as to bring the temperature of the receiver 43 close to the target receiver temperature, the controller 55 controls (adjusts) the amount of the refrigerant stored in the receiver 43 (the amount of the refrigerant flowing through the inside of the receiver 43). Thereby, the refrigerant temperature in the receiver 43 is controlled (adjusted). That is, the refrigerant temperature in the receiver 43 is made to the expected temperature (target receiver temperature) by adjusting the opening of the adjusting valve 44 to thereby control the density of the refrigerant in the receiver 43. This can bring the refrigerant amount stored in the receiver 43 to the proper amount. As a result, the amount of the circulated refrigerant can be made to be optimum. Note that the controller 55 is formed of, for example, a microcomputer.

[0062] As shown in Fig. 1, in the present embodiment, the receiver temperature detector 50 consists of a receiver thermistor 50a provided to the receiver 43, the air heat exchanger temperature detector 51 consists of an air heat exchange thermistor 51a provided to the evaporator 28, the suction pipe temperature detector 52 consists of a suction pipe thermistor 52a provided to the suction pipe 33, and the outside air temperature detector 53 consists of an outside air thermistor 53a. The discharge pipe 29 is also provided with a discharge pipe thermistor 56a for detecting the temperature of the discharge pipe.

[0063] Next, the driving operation of the heat pump type hot-water supply equipment (water heating operation) will be described.

[0064] First, the compressor is driven while the pump 13 for water circulation is also driven (operated). Then, stored water (hot water) flows out from the water intake 10 provided to the bottom of the hot-water reservoir tank

3. Then, the hot water flown out flows through the heat exchange path 14 of the circulation path 12. At this time, the hot water is heated (boiled) by the hydrothermal exchanger 26 which is a gas cooler. The heated hot water flows into the upper part of the hot-water reservoir tank 3 from the hot water inlet 11. By continuing this operation, hot water is stored in the hot-water reservoir tank 3.

[0065] It should be noted that under the current Japanese electricity rate system, the electricity rate of the night time is lower than that of the day time. Therefore, in order to reduce the cost, it is preferable that the heat pump type hot-water supply equipment is operated in the midnight time zone.

[0066] Further, the water heating operation of the heat pump type hot-water supply equipment is performed according to the flowchart shown in Fig. 3.

[0067] First, a user sets, for example, the tapping temperature by using a remote controller. Further, the outside air thermistor 53a detects the outside air temperature, and the temperature (data) detected is input into the controller 55.

[0068] Next, as shown as step S1, the target tapping temperature is determined (set) and the target temperature of the discharge pipe is determined (set).

[0069] Here, the required amount of the circulated refrigerant differs depending on the season, that is, depending on the outside air temperature. As such, in order to operate with the optimum amount of the circulated refrigerant, the target receiver temperature is determined (set) beforehand based on the outside air temperature detected and the past data (data obtained by the preliminary test or the like), and based on the target receiver temperature determined, the opening (initial opening) of the adjusting valve 44 is set, as shown as step S2.

[0070] Next, as shown as step S3, the target tapping temperature is controlled and the target temperature of the discharge pipe is controlled. The control of the target tapping temperature means that the tapping temperature is set to the target tapping temperature. The control of the target temperature of the discharge pipe means that the opening of the motor-operated expansion valve 27 is adjusted (controlled) to thereby set the temperature of the discharge pipe 29 to the target temperature of the discharge pipe.

[0071] Further, during operation, the receiver thermistor 50a, the air heat exchange thermistor 51a, the suction pipe thermistor 52a, and the outside air thermistor 53a detect the temperature of the receiver 43, the temperature of the air heat exchanger, the temperature of the suction pipe, and the outside air temperature, and then the detected temperatures (data) are input into the controller 55.

[0072] Here, when the outside air temperature becomes higher, it is required to increase the amount of the circulated refrigerant, that is, to reduce the amount of the refrigerant stored in the receiver 43. In order to reduce the refrigerant amount stored in the receiver 43,



the density of the refrigerant in the receiver 43 should be lowered, and in order to lower the density of the refrigerant in the receiver 43, the temperature of the receiver 43 should be raised. As such, in order to operate the equipment with the optimum amount of the circulated refrigerant when the outside air temperature becomes higher, the temperature of the receiver 43 should be raised. In turn, when the outside air temperature becomes lower, the temperature of the receiver 43 should be lowered.

[0073] Further, when the superheat degree of the refrigerant at the outlet of the evaporator 28 becomes larger, it is required to increase the amount of the circulated refrigerant, that is, to reduce the amount of the refrigerant stored in the receiver 43. Therefore, as same as the aforementioned, in order to operate the equipment with the optimum amount of the circulated refrigerant when the superheat degree becomes larger, the temperature of the receiver 43 should be raised. In turn, when the superheat degree becomes smaller, the temperature of the receiver 43 should be lowered.

[0074] Now, the controller 55 computes the superheat degree of the refrigerant at the outlet of the evaporator 28 based on the detected air heat exchanger temperature and the suction pipe temperature, and calculates the target receiver temperature based on the detected outside air temperature, the calculated superheat degree and the past data. Then, the controller 55 judges whether the target receiver temperature calculated coincides with the target receiver temperature having been set beforehand. If judges that the target receiver temperature calculated is different from the target receiver temperature set beforehand, the controller 55 corrects the target receiver temperature to the target receiver temperature which is calculated from the target receiver temperature set beforehand ("calculates the target receiver temperature" shown as step S4). This means that the optimum amount of the circulated refrigerant for the current operational state may not be obtained at the target receiver temperature set in step S2 in some cases, since the condensation load and the cooling load have been fluctuated. Therefore, in this step S4, the target receiver temperature, with which the amount of the circulated refrigerant is made to be optimum, is calculated.

[0075] Next, moving to step S5, the controller 55 compares the detected temperature of the receiver 43 with the target receiver temperature corrected. That is, in step S5, the detected temperature of the receiver 43 and the target receiver temperature (the target receiver temperature which has been corrected) are judged whether they coincide with each other.

[0076] If the detected temperature of the receiver 43 and the target receiver temperature corrected are judged that they coincide with each other, the operation for controlling the target tapping temperature and the operation for controlling the target temperature of the discharge pipe are continued (step S3).

[0077] In contrast, if the detected temperature of the

receiver 43 and the target receiver temperature corrected are judged to be different, the operation moves to step S6. Then, the controller 55 performs an EVB opening adjustment (opening adjustment of the adjusting valve 44) so as to adjust the refrigerant amount stored in the receiver 43. If the detected temperature of the receiver 43 is higher than the target receiver temperature corrected, the adjusting valve 44 is choked. If the detected temperature of the receiver 43 is lower than the target receiver temperature corrected, the adjusting valve 44 is released. With this step, the temperature of the receiver 43 can come close to the target receiver temperature corrected so that the amount of the circulated refrigerant can be made to the expected amount corresponding to the current operational state (operational condition).

[0078] For example, the optimum amount of the circulated refrigerant in the summer (the outside air temperature is about 32°C) is larger than the optimum amount of the circulated refrigerant in the winter (outside air temperature is about -5°C). Therefore, in the winter, the temperature of the receiver 43 is controlled so as to come close to the target receiver temperature of the winter, to thereby store in the receiver 43 the amount of the refrigerant corresponding to the difference between the optimum amount of the circulated refrigerant for the summer and the optimum amount of the circulated refrigerant for the winter. Thereby, the amount of the circulated refrigerant in the winter becomes less than the amount of the circulated refrigerant in the summer. On the other hand, in the summer, the temperature of the receiver 43 is controlled so as to come close to the target receiver temperature of the summer, to thereby cause the amount of the refrigerant stored in the receiver 43 during the winter to flow out. Thereby, the amount of the circulated refrigerant in the summer becomes larger than the optimum amount of the circulated refrigerant in the winter.

[0079] Fig. 6 shows the relationship among the outside air temperature, the superheat degree of the refrigerant at the outlet of the evaporator 28, the target receiver temperature, and the refrigerant amount stored in the receiver 43 (the amount of the refrigerant flowing through the inside of the receiver 43), which are obtained from experimentations using the heat pump type hot-water supply equipment according to the present embodiment. The heat pump type hot-water supply equipment used in the experimentations includes the receiver 43 with the capacity of 400cc and the pressure inside the receiver 43 is 11 Mpa.

[0080] As is obvious in Fig. 6, when the outside air temperature becomes higher, the target receiver temperature becomes higher. This is because that as the outside air temperature becomes higher, the amount of the circulated refrigerant must be increased, that is, the refrigerant amount in the receiver 43 must be reduced. In order to reduce the refrigerant amount in the receiver 43, the target receiver temperature must be raised. As

such, the target receiver temperature becomes higher as the outside air temperature becomes higher.

[0081] Further, as is obvious in Fig. 6, as the superheat degree becomes larger, the target receiver temperature becomes higher. This is because that as the superheat degree becomes larger, the amount of the circulated refrigerant must be increased, that is, the refrigerant amount in the receiver 43 must be reduced. In order to reduce the refrigerant amount in the receiver 43, the target receiver temperature must be raised. As such, the target receiver temperature becomes higher as the superheat degree becomes larger. By raising the target receiver temperature, the superheat degree becomes smaller.

[0082] In this way, the equipment can be operated with the amount of the circulated refrigerant corresponding to the season (condition) regardless of the fluctuation in the outside air temperature along with the season's transfer. Thereby, an excessive superheat operation and a wet operation can be prevented. Consequently, the reliability of the compressor 25 is improved. Further, by controlling the amount of the circulated refrigerant as described above, the heat pump type hot-water supply equipment having the refrigerant circuit R can exhibit the ability to the maximum.

[0083] Further, the controller 55 can adjust the refrigerant temperature in the receiver 43 by controlling the temperature of the receiver 43 so as to come close to the target receiver temperature set corresponding to, for example, the season. Thereby, the density of the refrigerant stored in the receiver 43 can be controlled, so that the refrigerant amount stored in the receiver 43 can be adjusted. Thus, the refrigerant amount stored in the receiver 43 can be adjusted to the amount corresponding to the season, so that the amount of the circulated refrigerant is made to the amount corresponding to the season. Therefore, an excessive superheat operation and a wet operation can be prevented.

[0084] Further, the controller 55 calculates the target receiver temperature based on the outside air temperature and the superheat degree serving as indexes for controlling the amount of the circulated refrigerant. Therefore, it is possible to ensure the amount of the circulated refrigerant to be the expected amount (for example, amount of the circulated refrigerant corresponding to the season).

[0085] Further, in step S4, the target receiver temperature is corrected based on two indexes which are the outside air temperature and the superheat degree. Therefore, it is possible to control the amount of the circulated refrigerant with higher precision.

[0086] Further, the controller 55 brings the temperature of the receiver 43 close to the target receiver temperature by adjusting the opening of the adjusting valve 44. Therefore, the amount of the circulated refrigerant can be controlled by such a simple control as adjusting the opening of the adjusting valve 44.

[0087] Further, the controller 55 corrects, from time to

time during operation, the target receiver temperature based on the outside air temperature and the superheat degree, while adjusting, from time to time during operation, the adjusting valve 44 to be the opening corresponding to the target receiver temperature adjusted. Thus, the temperature of the receiver 43 can surely come close to the target receiver temperature corrected. Thereby, the refrigerant amount stored in the receiver 43 can be made to the amount corresponding to, for example, the season, so that the amount of the circulated refrigerant can be made to the amount corresponding to the season. This can prevent an excessive superheat operation and a wet operation.

[0088] Further, since the adjusting valve 44 is provided to the second passage 46 of the bypass circuit 42, the controller 55 can surely control the refrigerant amount stored in the receiver 43 provided to the bypass circuit 42 by adjusting the opening of the adjusting valve 44. Therefore, the amount of the circulated refrigerant is ensured to be the expected amount.

[0089] Further, since the receiver 43 and the low-pressure refrigerant flowing through the passage 47 perform a heat exchange, the receiver 43 can be cooled by the low-pressure refrigerant. Therefore, the temperature of the receiver 43 can easily come close to the target receiver temperature without any additional cooler.

[0090] Although the aforementioned embodiment sets a target receiver temperature and then corrects the target receiver temperature based on the detected outside air temperature and the computed superheat degree, the target receiver temperature may be corrected (calculated) based solely on the outside air temperature or the superheat degree. Here, since the outside air temperature is detected by the outside air thermistor 53a, the outside air temperature can be detected without a calculation. Therefore, if the target receiver temperature is calculated based on the outside air temperature, it is possible to simplify the calculation for controlling the amount of the circulated refrigerant. Further, the magnitude of the superheat degree has a close relationship with the degree of the superheat operation. Therefore, if the target receiver temperature is calculated based on the superheat degree, the amount of the circulated refrigerant can be controlled with high precision.

[0091] Further, although the aforementioned embodiment shows processes from step S1 to step S6 in the flowchart of Fig. 3, step S4 and step S5 may be omitted. That is, the superheat degree may be calculated based on the temperature of the air heat exchanger and the temperature of the suction pipe, and based on the detected outside air temperature and the calculated superheat degree, the opening of the adjusting valve 44 may be determined. This enables to adjust the refrigerant amount stored in the receiver 43, whereby the amount of the circulated refrigerant can be made to the expected amount corresponding to the operational state. At this time, it is not required to calculate (correct) the target

receiver temperature, to compare the temperature of the receiver 43 with the calculated (corrected) target receiver temperature, and the like, which enable to simplify the control of the amount of the circulated refrigerant. Further, in the case of omitting step S4 and step S5, the opening of the adjusting valve 44 can be determined based on at least one of the outside air temperature or the superheat degree.

[0092] Further, the receiver 43 may be configured in such a manner as to cause the high-pressure refrigerant to flow and to cause the receiver 43 (the high-pressure refrigerant flown) and the low-pressure refrigerant to perform a heat exchange. Therefore, the first passage 45 of the bypass circuit 42 may be branched from the discharge pipe 29, the gas cooler 26 or the refrigerant passage 30, and the second passage 46 may be connected to the discharge pipe 29, the gas cooler 26 or the refrigerant passage 30 which are located downstream of the aforementioned branch portion. That is, the first passage 45 and the second passage 46 may be provided to the upstream side of the decompressing mechanism (motor-operated expansion valve) 27 in the high-pressure side of the refrigerant circuit R. However, the first passage 45 and the second passage 46 must be so formed as to generate a pressure difference between the first passage 45 and the second passage 46.

[0093] Further, the low-pressure refrigerant performing a heat exchange with the receiver 43 may be the low-pressure refrigerant flowing through the suction pipe 33. Moreover, in order to perform the heat exchange, the passages for the low-pressure refrigerant such as the refrigerant passage 31 and the suction pipe 33 may be formed along the outer surface of the receiver 43 as shown in Fig. 5. Moreover, the passages for the low-pressure refrigerant may be coiled to the outer peripheral of the receiver 43, although this is not shown.

[0094] As described above, although a specific embodiment of the present invention has been explained, this invention is not limited to the aforementioned embodiment and is able to be carried out with various changes within the scope of the invention. For example, the refrigerant circuit R can be applied to a refrigerant circuit of any type of refrigerating apparatus such as an air conditioning apparatus or a showcase, other than heat-pump type hot-water supply equipment. Further, as a refrigerant, a natural system refrigerant (supercritical refrigerant) other than carbon dioxide, such as ethylene, ethane or nitrogen oxide, may be used. Further, as a cooler S for cooling the receiver 43 (high-pressure refrigerant in the receiver 43), a fan device or other cooling devices may be used instead of using a low-pressure refrigerant, and moreover, a part of the evaporator 28 may also be used. Further, as the adjusting valve 44, not only a motor-operated valve but also a solenoid valve or other open/close valves may be used. Further, as the decompressing mechanism 27, not only a motor-operated expansion valve but also a capillary tube may be used. Further, the receiver 43 and the heat exchang-

er (liquid-gas heat exchanger) 34 shown in Fig. 1 may be arranged in reverse order.

## Industrial Applicability

[0095] As described above, the refrigerating apparatus according to the present invention is available for a heat source unit of heat-pump type hot-water supply equipment.

## Claims

### 1. A refrigerating apparatus comprising:

a supercritical freezing cycle (R) having a compressor (25) for compressing a refrigerant to a pressure higher than a critical pressure, a gas cooler (26), a decompressing mechanism (27) and an evaporator (28), and using as the refrigerant a natural system refrigerant;  
a receiver (43) provided to a high-pressure side of the supercritical freezing cycle (R);  
a receiver temperature detector (50a) for detecting a temperature of the receiver (43); and  
a controller (55) for controlling an amount of a circulated refrigerant by bringing the temperature of the receiver (43) detected by the receiver temperature detector (50a) close to a target receiver temperature.

### 2. The refrigerating apparatus as claimed in claim 1, further comprising an outside air temperature detector (53a) for detecting an outside air temperature, wherein

the controller (55) is so configured as to calculate the target receiver temperature based on the outside air temperature detected by the outside air temperature detector (53a).

### 3. The refrigerating apparatus as claimed in claim 1, further comprising a superheat degree detector (51a, 52a, 55) for detecting a superheat degree of the refrigerant at an outlet of the evaporator (28), wherein

the controller (55) is so configured as to calculate the target receiver temperature based on the superheat degree detected by the superheat degree detector (51a, 52a, 55).

### 4. The refrigerating apparatus as claimed in claim 1, further comprising:

an outside air temperature detector (53a) for detecting an outside air temperature; and  
a superheat degree detector (51a, 52a, 55) for detecting a superheat degree of the refrigerant at an outlet of the evaporator (28), wherein

the controller (55) is so configured as to calculate the target receiver temperature based on the outside air temperature detected by the outside air temperature detector (53a) and the superheat degree detected by the superheat degree detector (51a, 52a, 55).

5. The refrigerating apparatus as claimed in claim 1, further comprising an adjusting valve (44) for adjusting an amount of the refrigerant flowing through an inside of the receiver (43), wherein the controller (55) is so configured as to adjust an opening of the adjusting valve (44) to thereby bring the temperature of the receiver (43) detected by the receiver temperature detector (50a) close to the target receiver temperature.
6. A refrigerating apparatus comprising:
  - a supercritical freezing cycle (R) having a compressor (25) for compressing a refrigerant to a pressure higher than a critical pressure, a gas cooler (26), a decompressing mechanism (27) and an evaporator (28), and using as the refrigerant a natural system refrigerant;
  - a receiver (43) provided to a high-pressure side of the supercritical freezing cycle (R);
  - an adjusting valve (44) for adjusting an amount of the refrigerant flowing through an inside of the receiver (43);
  - an outside air temperature detector (53a) for detecting an outside air temperature; and
  - a controller (55) for controlling an amount of a circulated refrigerant by adjusting an opening of the adjusting valve (44) based on the outside air temperature detected by the outside air temperature detector (53a).
7. A refrigerating apparatus comprising:
  - a supercritical freezing cycle (R) having a compressor (25) for compressing a refrigerant to a pressure higher than a critical pressure, a gas cooler (26), a decompressing mechanism (27) and an evaporator (28), and using as the refrigerant a natural system refrigerant;
  - a receiver (43) provided to a high-pressure side of the supercritical freezing cycle (R);
  - an adjusting valve (44) for adjusting an amount of the refrigerant flowing through an inside of the receiver (43);
  - a superheat degree detector (51a, 52a, 55) for detecting a superheat degree of the refrigerant at an outlet of the evaporator (28); and
  - a controller (55) for controlling an amount of a circulated refrigerant by adjusting an opening of the adjusting valve (44) based on the superheat degree detected by the superheat degree

detector (51a, 52a, 55).

8. A refrigerating apparatus comprising:

- a supercritical freezing cycle (R) having a compressor (25) for compressing a refrigerant to a pressure higher than a critical pressure, a gas cooler (26), a decompressing mechanism (27) and an evaporator (28), and using as the refrigerant a natural system refrigerant;
- a receiver (43) provided to a high-pressure side of the supercritical freezing cycle (R);
- an adjusting valve (44) for adjusting an amount of the refrigerant flowing through an inside of the receiver (43);
- an outside air temperature detector (53a) for detecting an outside air temperature;
- a superheat degree detector (51a, 52a, 55) for detecting a superheat degree of the refrigerant at an outlet of the evaporator (28); and
- a controller (55) for controlling an amount of a circulated refrigerant by adjusting an opening of the adjusting valve (44) based on the outside air temperature detected by the outside air temperature detector (53a) and the superheat degree detected by the superheat degree detector (51a, 52a, 55).

9. The refrigerating apparatus as claimed in claim 1, further comprising, an adjusting valve (44) for adjusting an amount of the refrigerant flowing through an inside of the receiver (43), and an outside air temperature detector (53a) detecting an outside air temperature, wherein

the controller (55) is so configured as to correct, from time to time during operation, the target receiver temperature based on the outside air temperature, and adjust, from time to time during operation, an opening of the adjusting valve (44), to thereby bring the temperature of the receiver (43) close to the target receiver temperature corrected.

10. The refrigerating apparatus as claimed in claim 1, further comprising, an adjusting valve (44) for adjusting an amount of the refrigerant flowing through an inside of the receiver (43), and a superheat degree detector (51a, 52a, 55) for detecting a superheat degree of the refrigerant at an outlet of the evaporator (28), wherein

the controller (55) is so configured as to correct, from time to time during operation, the target receiver temperature based on the superheat degree, and adjust, from time to time during operation, an opening of the adjusting valve (44), to thereby bring the temperature of the receiver (43) close to the target receiver temperature corrected.

11. The refrigerating apparatus as claimed in claim 1,

further comprising, an adjusting valve (44) for adjusting an amount of the refrigerant flowing through an inside of the receiver (43), an outside air temperature detector (53a) detecting an outside air temperature, and a superheat degree detector (51a, 52a, 55) for detecting a superheat degree of the refrigerant at an outlet of the evaporator (28), wherein

the controller (55) is so configured as to correct, from time to time during operation, the target receiver temperature based on the outside air temperature and the superheat degree, and adjust, from time to time during operation, an opening of the adjusting valve (44), to thereby bring the temperature of the receiver (43) close to the target receiver temperature corrected.

12. The refrigerating apparatus as claimed in claim 5, further comprising a bypass circuit (42) for connecting an intermediate portion in the high-pressure side of the supercritical freezing cycle (R) and a downstream portion located at a downstream side of the intermediate portion, wherein

the receiver (43) is provided to the bypass circuit (42), and

the adjusting valve (44) is provided in between the receiver (43) and the downstream portion in the bypass circuit (42).

13. The refrigerating apparatus as claimed in claim 6, further comprising a bypass circuit (42) for connecting an intermediate portion in the high-pressure side of the supercritical freezing cycle (R) and a downstream portion located at a downstream side of the intermediate portion, wherein

the receiver (43) is provided to the bypass circuit (42), and

the adjusting valve (44) is provided in between the receiver (43) and the downstream portion in the bypass circuit (42).

14. The refrigerating apparatus as claimed in claim 7, further comprising a bypass circuit (42) for connecting an intermediate portion in the high-pressure side of the supercritical freezing cycle (R) and a downstream portion located at a downstream side of the intermediate portion, wherein

the receiver (43) is provided to the bypass circuit (42), and

the adjusting valve (44) is provided in between the receiver (43) and the downstream portion in the bypass circuit (42).

15. The refrigerating apparatus as claimed in claim 8, further comprising a bypass circuit (42) for connecting an intermediate portion in the high-pressure side of the supercritical freezing cycle (R) and a downstream portion located at a downstream side of the intermediate portion, wherein

the receiver (43) is provided to the bypass circuit (42), and

the adjusting valve (44) is provided in between the receiver (43) and the downstream portion in the bypass circuit (42).

16. The refrigerating apparatus as claimed in claim 1, further comprising a heat exchanger (S) for causing a heat exchange between the receiver (43) and a low-pressure refrigerant flowing through a passage (47) in a low-pressure side of the supercritical freezing cycle (R).

17. The refrigerating apparatus as claimed in claim 6, further comprising a heat exchanger (S) for causing a heat exchange between the receiver (43) and a low-pressure refrigerant flowing through a passage (47) in a low-pressure side of the supercritical freezing cycle (R).

18. The refrigerating apparatus as claimed in claim 7, further comprising a heat exchanger (S) for causing a heat exchange between the receiver (43) and a low-pressure refrigerant flowing through a passage (47) in a low-pressure side of the supercritical freezing cycle (R).

19. The refrigerating apparatus as claimed in claim 8, further comprising a heat exchanger (S) for causing a heat exchange between the receiver (43) and a low-pressure refrigerant flowing through a passage (47) in a low-pressure side of the supercritical freezing cycle (R).

FIG. 1

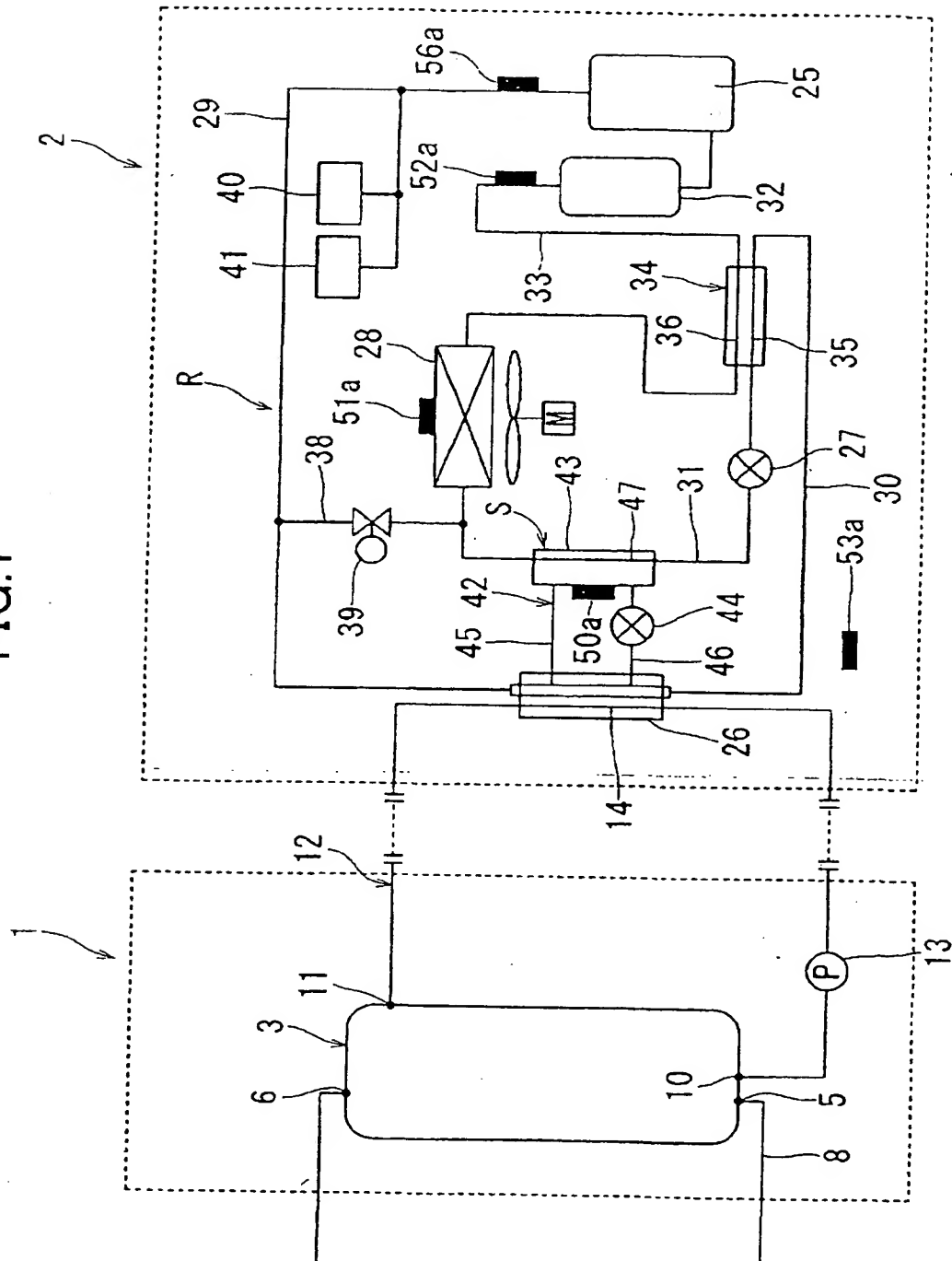


FIG.2

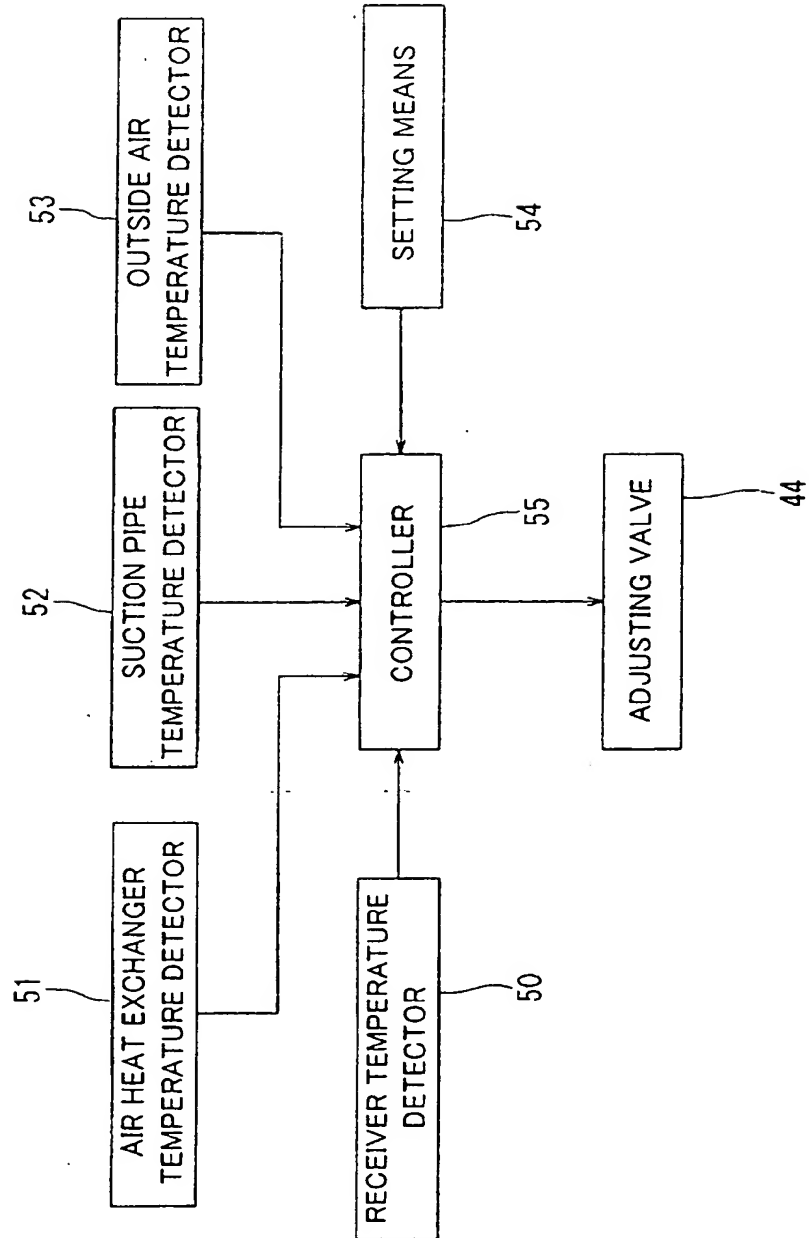




FIG.3

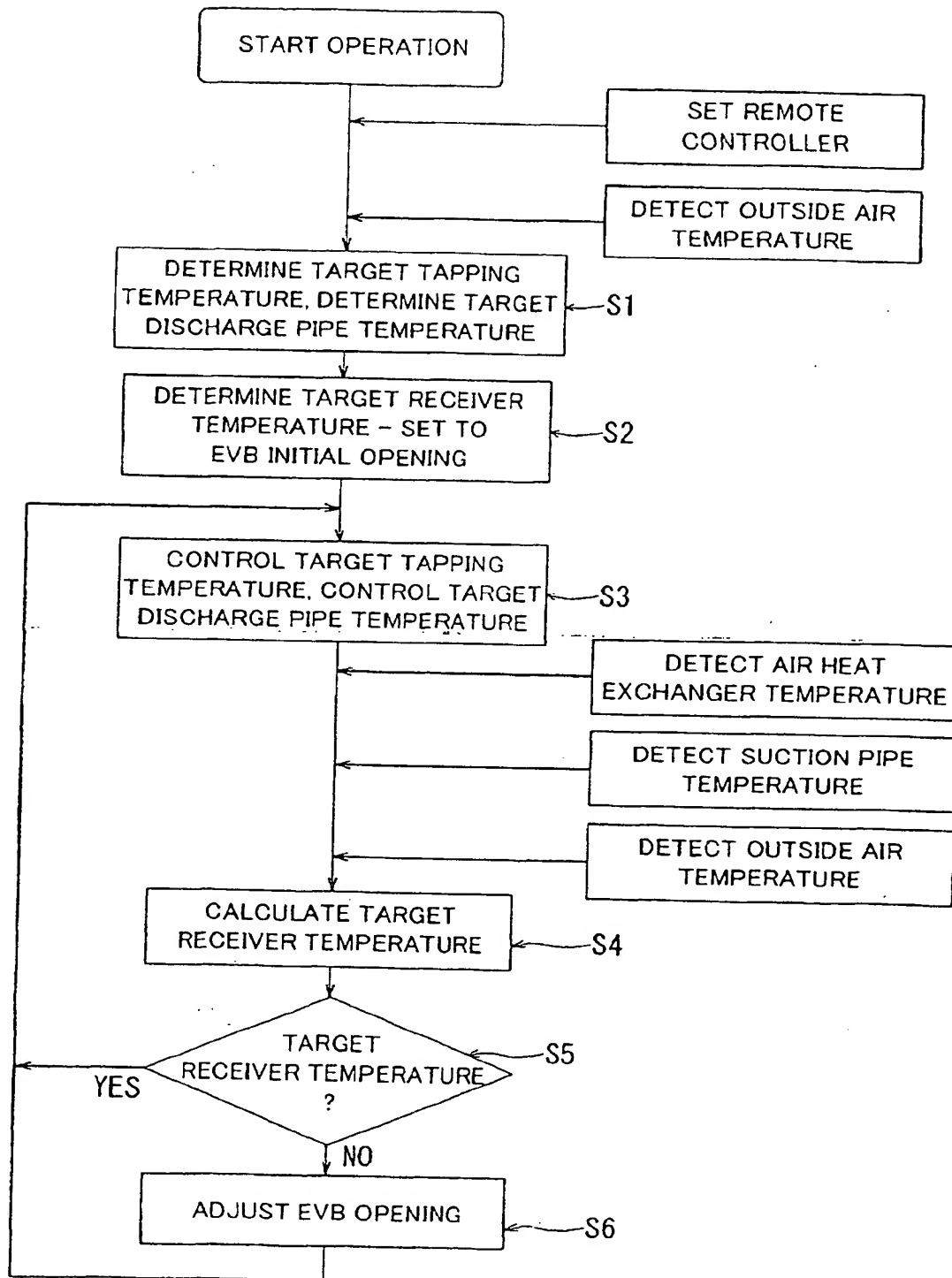


FIG.4

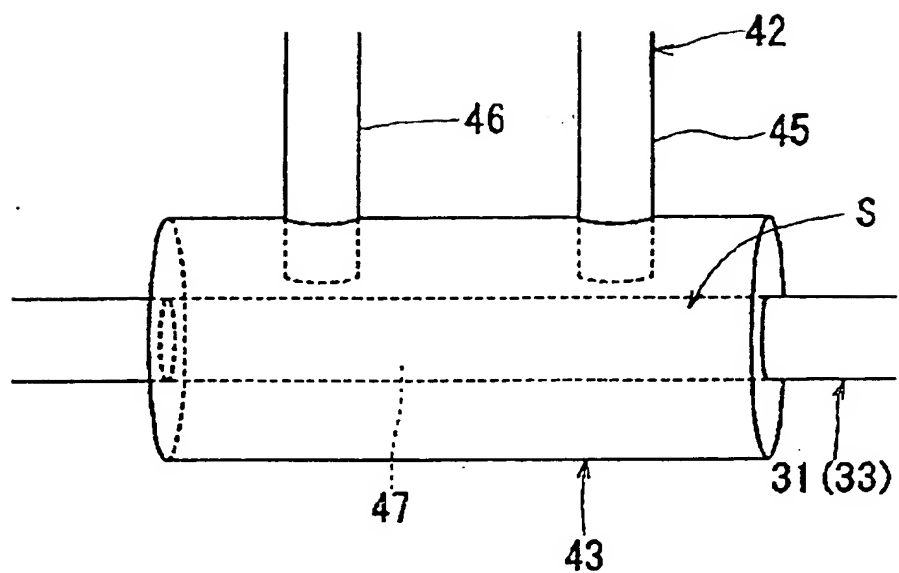


FIG.5

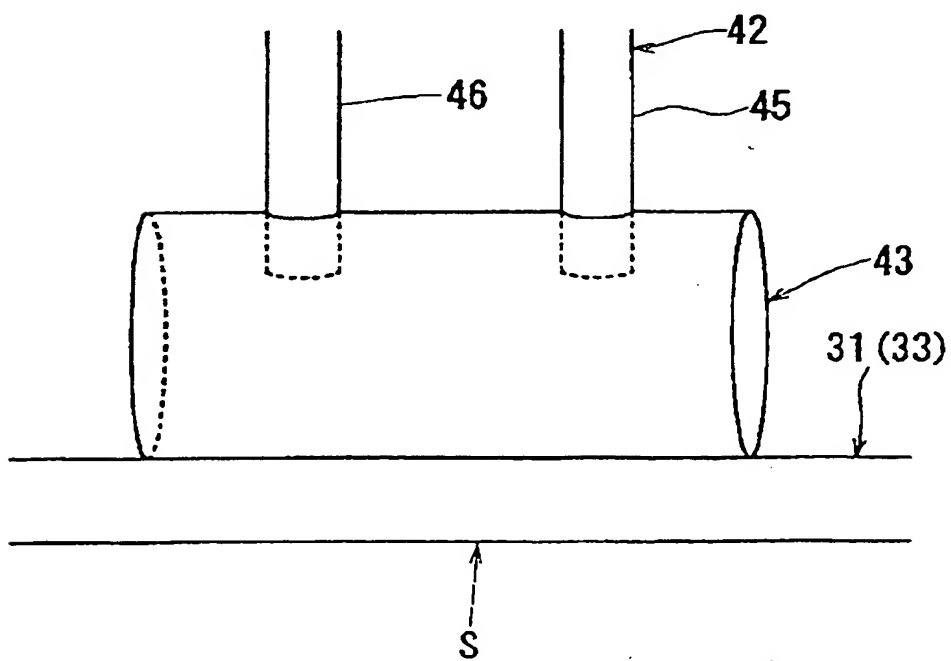


FIG.6

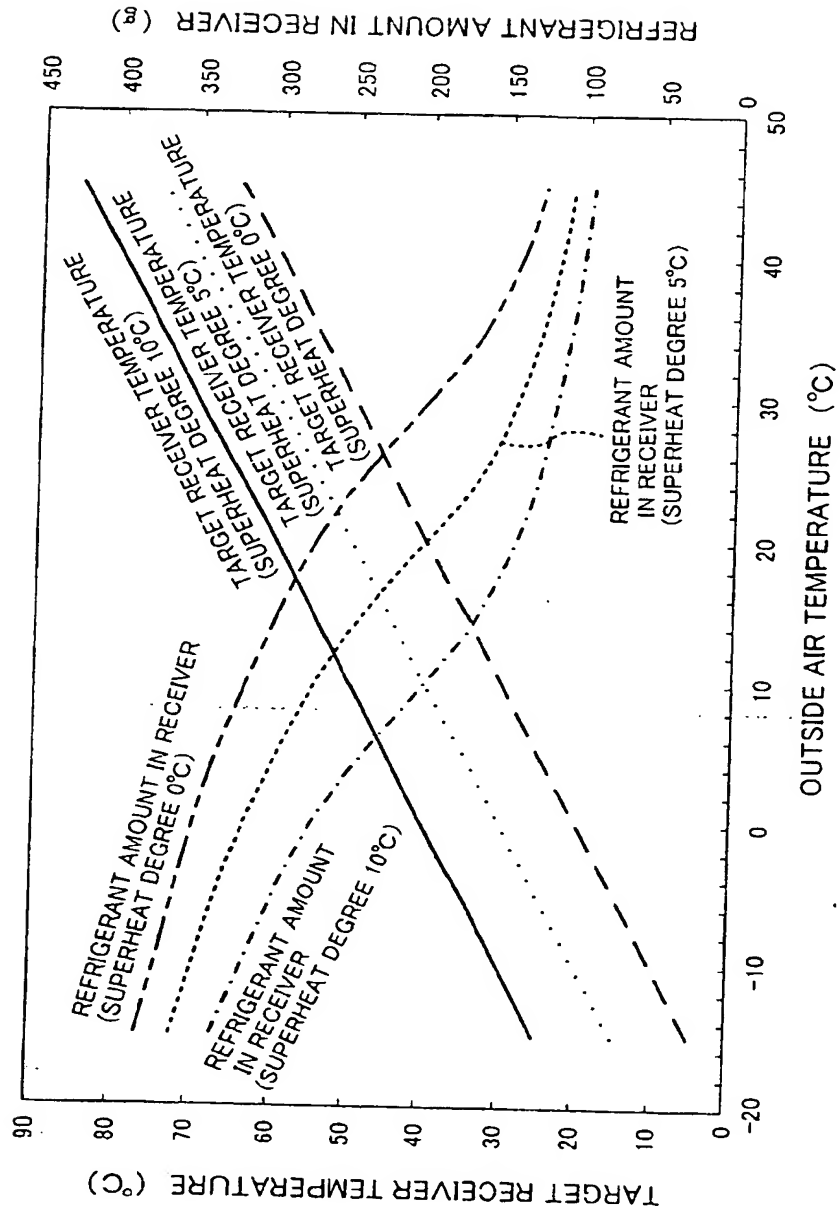
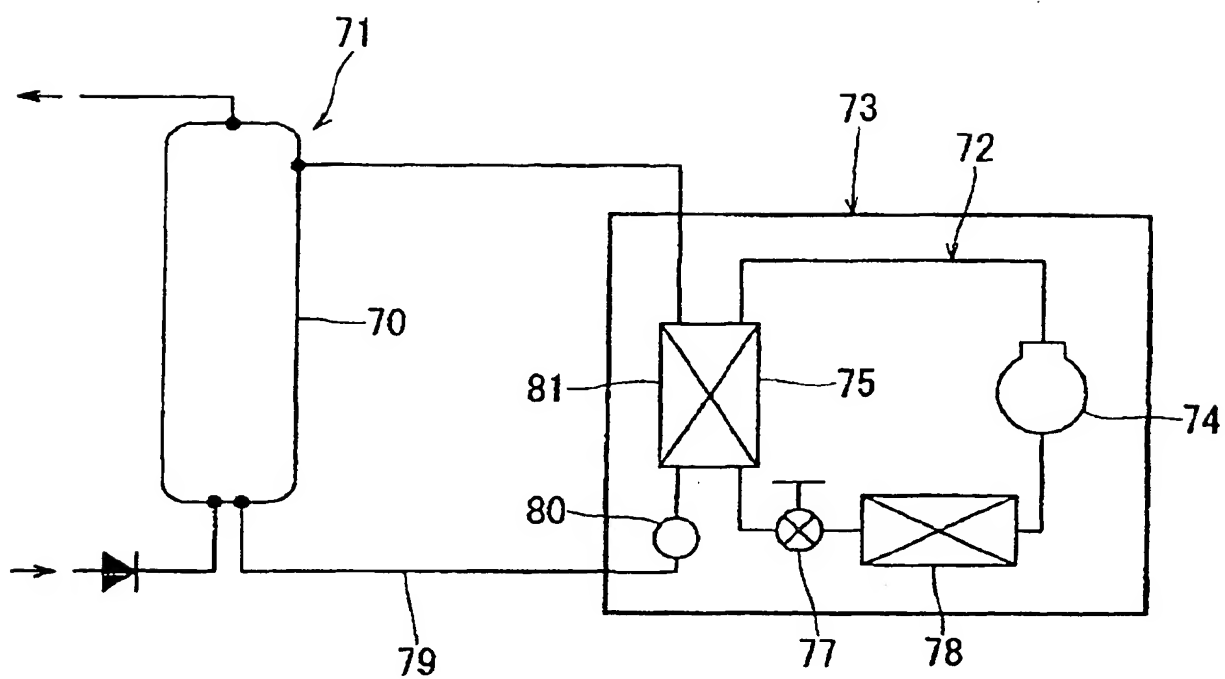


FIG.7



## INTERNATIONAL SEARCH REPORT

International application No.

PCT/JP02/11122

A. CLASSIFICATION OF SUBJECT MATTER  
Int.Cl<sup>7</sup> F24H1/00, F25B1/00

According to International Patent Classification (IPC) or to both national classification and IPC

## B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)  
Int.Cl<sup>7</sup> F24H1/00, F25B1/00

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched  
Jitsuyo Shinan Koho 1922-1996 Jitsuyo Shinan Toroku Koho 1996-2003  
Kokai Jitsuyo Shinan Koho 1971-2003 Toroku Jitsuyo Shinan Koho 1994-2003

Electronic data base consulted during the international search (name of data base and, where practicable, search terms used)

## C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
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A	AU 2504195 A1 (Mitsubishi Denki Kabushiki Kaisha), 01 February, 1996 (01.02.96), & JP 8-35725 A	1-19
A	JP 2000-266415 A (Bosch Automotive Systems Corp.), 29 September, 2000 (29.09.00), (Family: none)	1-19
A	EP 1059495 A2 (Mitsubishi Heavy Industries, Ltd.), 13 December, 2000 (13.12.00), & JP 2000-346472 A & NO 20002839 A & CN 1278052 A & US 6343486 A	1-19

☒ Further documents are listed in the continuation of Box C. ☐ See patent family annex.

* Special categories of cited documents:	"T" later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention
"A" document defining the general state of the art which is not considered to be of particular relevance	"X" document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step when the document is taken alone
"E" earlier document but published on or after the international filing date	"Y" document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art
"L" document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified)	"Z" document member of the same patent family
"O" document referring to an oral disclosure, use, exhibition or other means	
"P" document published prior to the international filing date but later than the priority date claimed	

Date of the actual completion of the international search  
30 January, 2003 (30.01.03)

Date of mailing of the international search report  
12 February, 2003 (12.02.03)

Name and mailing address of the ISA/  
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## INTERNATIONAL SEARCH REPORT

International application No.

PCT/JP02/11122

C (Continuation). DOCUMENTS CONSIDERED TO BE RELEVANT		
Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
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E	JP 2002-277078 A (Mitsubishi Electric Corp.), 25 September, 2002 (25.09.02), (Family: none)	1-19

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